Thermal quench and asymmetric wall force in ITER disruptions

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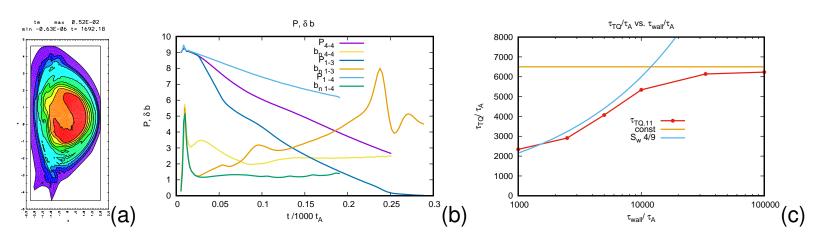
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Outline

The long ITER resitive wall penetration time τ_{wall} can have mitigating effects on TQ, REs, and asymmetric wall force

- Thermal quench
 - TQ time can depend on au_{wall} because of resistive wall tearing mode
- Asymmetric wall force depends on $S_{wall} = \tau_{wall}/\tau_A$
 - Cold disruptions : small force when CQ time $au_{CQ} \leq au_{wall}$
 - Hot disruptions : small force when $S_{wall} >> 100$.
- REs in cold disruptions
 - Runaway electrons can cause large wall force when RE current fraction ≈ 1 .
 - Longer TQ time can reduce RE current fraction

Thermal Quench Simulations



Simulations with M3D initialized with ITER [Strauss, PoP 2018] inductive Scenario 2 15 MA with current profile modified to represent MGI mitigation. Current set to zero outside q=2 magnetic surface [Izzo 2008], keeping total current unchanged. Temperature also lowered outside the q=2 surface, increasing the resistivity which varied as $T^{-3/2}$. This made plasma MHD unstable. Parallel thermal conduction assumed with $T_e=100eV$ at the wall. In the simulations $S=10^6$ initially on axis.

(a)
$$T$$
 at $t = 2163\tau_A$, $S_{wall} = 10^3$.

(b) P history for cases, $S_{wall}=10^3, 2.5\times 10^3, 10^4$, showing normal asymmetric magnetic field at the wall b_n as a function of time. As b_n increases in time, P falls more rapidly. (c) normalized TQ time τ_{TQ}/τ_A vs. S_{wall} Fit to $\tau_{TQ}\propto S_{wall}^{4/9}$, suggests a RWTM [Finn, 1995].

Thermal Quench with RWTM

$$\frac{\partial T}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} r(\kappa_{\parallel} b_r^2 + \kappa_{\perp}) \frac{\partial T}{\partial r} \tag{1}$$

where b_r is the normalized asymmetric normal magnetic field, assuming circular flux surfaces for simplicity. Integrating, the total temperature is given by

$$\frac{\partial \langle T \rangle}{\partial t} = a(\kappa_{\parallel} b_r^2 + \kappa_{\perp}) T' \tag{2}$$

where $\langle T \rangle = \int Tr dr$, $T' = \partial T/\partial r(a)$, $c_1 = \langle T \rangle/(a^3T')$.

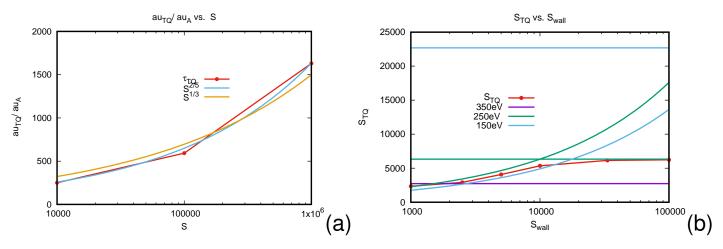
$$\frac{c_1 a^2}{\tau_{TQ}} = \kappa_{\parallel} [b_0^2 + b_2^2 \exp(\gamma_{RW} t)] + \kappa_{\perp} + \frac{\gamma_{RW}}{k_{\perp}^2}$$
 (3)

where the last term is quasilinear diffusion, and $\gamma_{RW}\tau_A \propto S^{-1/3}S_{wall}^{-4/9}$. Then obtain the *ad hoc* formula

$$au_{TQ} pprox rac{c_1 au_A}{c_0 S^{-1/3} S_{wall}^{-4/9} + \hat{\kappa}_\perp + \hat{\kappa}_\parallel b_0^2}$$
 (4)

where $\hat{\kappa}_{\parallel} = \kappa_{\parallel}/(a^2\tau_A)$, $\hat{\kappa}_{\perp} = \kappa_{\perp}/(a^2\tau_A)$, with $c_0 = \mathcal{O}(1)$.

TQ Timescales



- (a) τ_{TQ} for cases with $S=10^4, 10^5, 10^6,$ with $S_{wall}=10^4, \hat{\kappa}_{\parallel}=10, \hat{\kappa}_{\perp}=10^{-4}.$ The scaling is $S_{TQ}\approx S^{1/3}$. This gives $S_{TQ}=\tau_{TQ}/\tau_{A}=0.7S_{w}^{4/9}S^{1/3}.$
- (b) effect of varying T_e on κ_{\parallel} and S_{TQ} .

$$t_{TQ} \approx 1/(\hat{\kappa}_{\parallel}b_0^2) \approx 10^4 \tau_A = 10ms, b_0 \approx 3 \times 10^{-3}, T_e \approx 100eV.$$

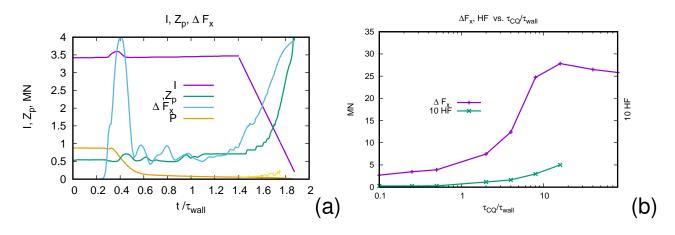
If
$$c_0 \approx 1/3$$
, $S = S_{wall} = 10^4$, then $t_{TQ} \approx S^{1/3} S_{wall}^{4/9} \approx 2ms$.

If TQ time is due to RWTMs, then $\tau_{TQ} \propto S_{wall}^{4/9}$ is about 6 times longer in ITER than in JET.

This could reduce thermal loading and RE generation.

ITER cold disruptions - asymmetric wall force

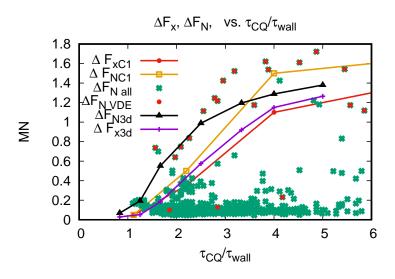
• cold disruptions - TQ precedes VDE and CQ. ΔF_x depends on τ_{CQ}/τ_{wall} . For expected ITER $\tau_{CQ}/\tau_{wall} < 1 \ \Delta F_x \approx 5 MN$.



- (a) Time history of I, Z_p , ΔF_x , P in wall time units [Strauss, 2018]. Simulation with $\tau_{CQ}/\tau_{wall}=1/2$
- (b) ΔF_x vs. τ_{CQ}/τ_{wall} with $\Delta F_x < 30MN$. Also shown is halo fraction HF.

Sideways wall force in JET disruptions

Simulations were done with M3D and recently with M3DC1 codes. The runs were initialized with a reconstruction of JET shot 71985. The current quench time τ_{CQ} was controlled by an applied electric field. The wall force is quenched for $\tau_{CQ} \leq \tau_{wall}$.

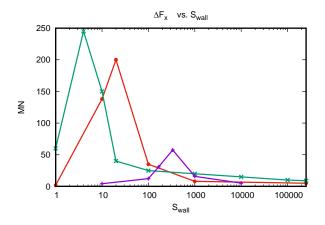


Solid curves: M3D and M3DC1 simulations where τ_{CQ}/τ_{wall} was varied. Plots of asymmetric wall force ΔF_x and Noll force $\Delta F_N = \pi B \Delta M_{IZ}$. ΔF_{xC1} , M3DC1 wall force, ΔF_{NC1} , M3DC1 Noll force, ΔF_{xm3} , M3D wall force, ΔF_{Nm3} , M3D Noll force.

Comparison with data: dots: ΔF_N and τ_{CQ} calculated for all JET shots in ILW disruption database, 2011 - 2016, labeled ΔF_{NJET} . Points "VDE" are VDE shots, and all shots. (JET Data discussed with E. Joffrin and S. Gerasimov and presented at ITPA meeting, Daejeong, Korea, April 2019)

ITER hot disruptions

• hot disruptions - VDE precedes TQ and CQ ΔF_x is maximum for $\gamma \tau_{wall} \sim 1$. In ITER $\gamma \tau_{wall} >> 1$ and ΔF_x is small.



asymmetric force in hot disruption simulations [Strauss et al. NF 2013] with $\Delta F_x < 60MN$. VDE caused plasma and flux to scrape off at the wall, until the edge $q \approx 2$. Also shown are "extra - hot" disruption with $\Delta F_x < 200, 250MN$. ΔF_x vs. S_{wall} . They were produced with 2D VDE of model MGI equilibria, then evolving in 3D.

For ITER relevant S_{wall} the force is small, unless there are REs with $au_{CQ} >> au_{wall}$

Runaway Electrons - Fluid model

If REs carry the current, it is possible that $\tau_{CQ} >> \tau_{wall}$. MHD simulations were extended by adding RE fluid model. Runaway fluid equations are

[Helander 2007],[Cai and Fu 2015]

$$\frac{1}{c}\frac{\partial\psi}{\partial t} = \nabla_{\parallel}\Phi - \eta(J_{\parallel} - J_{\parallel RE}) \tag{5}$$

and $J_{\parallel RE}$ is the RE current density. The RE continuity equation can be expressed,

assuming the REs have speed c

$$\frac{\partial J_{\parallel RE}}{\partial t} \approx -c\mathbf{B} \cdot \nabla \left(\frac{J_{\parallel RE}}{B}\right) + S_{RE} \tag{6}$$

where S_{RE} in the following is a model source term.

$$S_{RE} = \alpha(t)(J_{\parallel} - J_{\parallel RE})J_{\parallel RE} > 0 \tag{7}$$

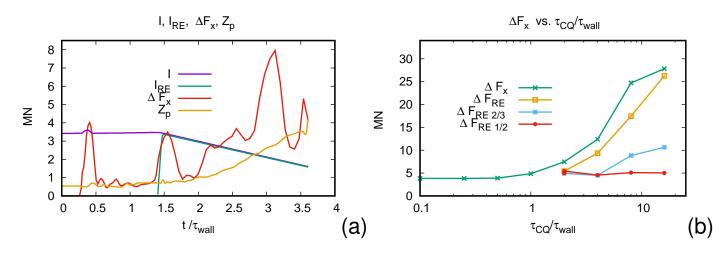
Approximately

$$\mathbf{B} \cdot \nabla \left(\frac{J_{\parallel RE}}{B} \right) = \mathcal{O}(v_A/c) \approx 0$$
 (8)

which is solved similarly to electron temperature, like a bounce average method.

ITER REs

With REs, 2 quantities determine wall force, τ_{CQ}/τ_{wall} and I_{REmax}/I_{p0} .



(a) ΔF_x , I, I_{RE} , and Z_p as functions of time t/τ_{wall} , for $I_{RE}=I_0$. (b) ΔF_x as a function of τ_{CQ}/τ_{wall} . Also shown are ΔF_{REa} , where a=1,2/3,1/2. The wall force depends on the ratio of RE current to initial current.

If $I_{RE}/I_0 \le 1/2$, the force is small.

If $I_{RE}/I_0 = 1$, the force is the same as having a long CQ time.

Summary

- ullet Long ITER au_{wall} has a mitigating effect on disruptions
- TQ time can depend on RWTM. In ITER, TQ time might be 10ms.
 - reduce thermal load rate
 - reduce RE generation rate
- ITER asymmetric wall force is small in cold and hot disruptions
 - cold disruptions TQ precedes VDE. Force is small for $\tau_{CQ} \leq \tau_{wall}$.
 - hot disruptions VDE precedes TQ, CQ. Force is small for $\gamma \tau_{wall} >> 1$
- REs
 - can affect cold disruptions, probably not relevant in hot disruptions
 - If ratio of RE current to initial current, $I_{RE}/I_{p0} \approx 1$, the force can be large.